

116.(D) $n_T = n_1 + n_2 + n_3 + \dots$

$$\frac{P_T \cdot V_T}{RT} = \frac{P_1 V_1}{RT} + \frac{P_2 V_2}{RT} + \dots = \sum P_i V_i$$

$$P_T V_T = \sum P_i V_i = 2PV + \frac{P \cdot V}{2} + \frac{P}{2} \cdot \frac{V}{4} + \frac{P}{4} \cdot \frac{V}{8} + \dots = 2PV \left[1 + \frac{1}{4} + \frac{1}{16} + \frac{1}{64} + \dots \right]$$

$$P_T V_T = 2PV \frac{1}{1 - \frac{1}{4}} = 2PV \frac{4}{3}$$

$$V_T = V_1 + V_2 + V_3 + \dots = V + \frac{V}{2} + \frac{V}{4} + \frac{V}{8} + \dots = V \left[1 + \frac{1}{2} + \dots \right] = V \frac{1}{1 - \frac{1}{2}} = 2V$$

$$\therefore P_T \cdot 2V = 2PV \frac{4}{3} \Rightarrow P_T = \frac{4}{3}P$$

117.(ABD) (A) $\therefore$ area under the curve gives fraction of molecules and total area is constant

(B) u_{mp} decreases with decrease in temperature

(C) T_2 is higher temperature

(D) As seen from graph; $\therefore$ A, B, D

118.(A) $\left(P + \frac{a}{V^2} \right) V = RT$

$$PV + \frac{a}{V} = RT \quad \text{or} \quad \frac{PV}{RT} + \frac{a}{RTV} = 1 \quad \text{or} \quad \frac{PV}{RT} = \left(1 - \frac{a}{RTV} \right) = Z$$

119.(D) On moving from region (II) to region (I), pressure tends to zero. So, $Z \rightarrow 1$

120.(B) $P_{\text{Total}} = \frac{dRT}{M_0} \Rightarrow M_0 = \frac{dRT}{P_T} = \frac{1.24 \times 0.0821 \times 300}{760 / 760} \Rightarrow M_0 = 30.54$

' M_0 ' here is the molar mass of air

$$M_0 = X_{N_2} M_{N_2} + X_{O_2} M_{O_2} = X_{N_2} M_{N_2} + (1 - X_{N_2}) M_{O_2}$$

$$30.54 = X_{N_2} (M_{N_2} - M_{O_2}) + M_{O_2} = X_{N_2} (28 - 32) + 32$$

$$30.54 - 32 = -4 X_{N_2}$$

$$0.365 = X_{N_2}$$

$$P_{N_2} = X_{N_2} P_T = 0.365 \times 1 \text{ atm} = 0.365 \text{ atm}$$

121.(C) $V_{\text{rms}} = \sqrt{\frac{3RT}{M}} = \frac{(V_{\text{rms}})_{H_2}}{(V_{\text{rms}})_{N_2}} = \sqrt{\frac{T_{H_2} \times \frac{M_{N_2}}{M_{H_2}}}{T_{N_2}}}; \quad (V_{\text{rms}})_{H_2} = \sqrt{5} (V_{\text{rms}})_{N_2}$

$$\therefore \frac{(V_{\text{rms}})_{H_2}}{(V_{\text{rms}})_{N_2}} \times \sqrt{5} = \sqrt{\frac{T_{H_2} \times \frac{M_{N_2}}{M_{H_2}}}{T_{N_2}}};$$

$$\frac{\sqrt{5}}{1} = \sqrt{\frac{T_{H_2} \times 14}{T_{N_2}}} \Rightarrow 5 = \frac{T_{H_2} \times 14}{T_{N_2}}$$

$$T_{N_2} \times 5 = T_{H_2} \times 14 \quad \therefore T_{N_2} > T_{H_2}$$

122.(D) $\frac{n'_{\text{He}}}{n'_{\text{CH}_4}} = \frac{1}{2} \sqrt{\frac{16}{4}} = \frac{1}{1}$

$$\frac{n'_{\text{He}}}{n'_{\text{SO}_2}} = \frac{1}{3} \sqrt{\frac{64}{4}} = \frac{4}{3}$$

$$n'_{\text{He}} : n'_{\text{CH}_4} : n'_{\text{SO}_2} = 4 : 4 : 3$$

123.(B) $P = \frac{1}{3} \frac{n m c^2}{V} = \frac{1}{3} \times \frac{6 \times 10^{22} \times 10^{-24} \times (100)^2}{10 \times 10^{-3}} = 2 \times 10^4 \text{ Pa}$

124.(B) Moles ratio $= \frac{n_{\text{He}}}{n_{\text{N}_2}} = \frac{w/4}{w/28} = \frac{7}{1}$

$$\text{Ratio of translational K.E.} = \frac{n_{\text{He}} \cdot T_{\text{He}}}{n_{\text{N}_2} \cdot T_{\text{N}_2}} = \frac{7}{1} \times \frac{300}{700} = 3 : 1$$

125.(C) $d_A = 2d_B$; $2M_A = M_B$; $PM = dRT$

$$\frac{P_A}{P_B} \times \frac{M_A}{M_B} = \frac{d_A}{d_B} \times \frac{RT}{RT} \Rightarrow \frac{P_A}{P_B} \times \frac{1}{2} = 2 \Rightarrow \frac{P_A}{P_B} = \frac{4}{1}$$